# Electrochemical Impedance Spectroscopy 

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WonATech

$Z I V \in L \wedge B$

## Nomenclature : EIS

- Electrochemical?
- In electrochemistry, everything of interest takes place at the interface between electrode \& electrolyte!
- Controlling REDOX by Potentiostat/galvanostat
- Impedance?
- AC circuit theory describes the response of a circuit to an alternating current or voltage as a function of frequency
- Impedance is a totally complex resistance encountered when a current flows through a circuit made of resistors, capacitors, or inductors, or any combination of these
- Ohm's Law, V = R •I $\rightarrow \mathrm{V}=\mathrm{Z} \cdot \mathrm{I}$ (complex number Z )
- Spectroscopy?
- No Quantum Process
- Small Perturbation $\rightarrow$ Response


## Excitations used in E'chem Techniques

1. DC


CA, CC, CP
Potentiostatic
2. Sweep
LSV, Tafel, PD, LPR

3. Pulse
4. Sine


# Electrochemical Interface and Electrochemical Process 

## Electrochemical Interface



- Everything happens at the interface
- Charge Transfer $\Rightarrow R_{c t}$
- $\mathrm{R}_{\mathrm{ct}} \sim 1 / \mathrm{i}_{0}$
- Butler-Volmer Equation
- Diffusion Layer $\Rightarrow \mathrm{W}$
- Bulk Electrolyte $\Rightarrow R_{\text {serr }} R_{\Omega}$
- Double Layer $\Rightarrow C_{\text {dl }}$
- Non-Faradaic Process


## Randles' Circuit



## Process of Energy Storage in Electrochemical System

## Common Steps

- Ionic charge conduction through electrolyte in pores of active layer
- Electronic charge conduction through conductive part of active layer
- Electrochemical reaction on the interface of active material particles including electron transfer
- Diffusion of ions or neutral species into or out of electrochemical reaction zone.



## Impedance Spectra of a Li-ion battery

Impedance Spectra upon cycling


Nyquist Plot vs. level of discharge


CF)Discharge curve upon cycling


Effect of temperature


## Circuit Elements (1)

## Basic Circuit Elements

| Resistor | $I(t)=I_{0} e^{i \omega x}$ |  |  |
| :---: | :---: | :---: | :---: |
| -W- | $E=R I$ | $\overrightarrow{E=Z \times I}$ | $Z=R$ |
| Inductor |  | $I(t)=I_{0}{ }^{i e^{\prime \prime}}$ |  |
| $\cdots$ | $E=L \frac{d I}{d t}$ | $\overrightarrow{E=Z \times I}$ | $Z=j a L$ |
| Capacitor | $=\frac{Q}{C}=\frac{1}{C} \int$ | $\begin{aligned} & I(t)=I_{0} e^{i e x} \\ & t \underbrace{}_{E=Z \times I} \\ & = \end{aligned}$ | $=\frac{1}{j \omega C}=$ |

## AC Current, Voltage, and Impedance

Voltage $\quad E(\omega)=E_{o} \cos (\omega t)$

$$
=E_{o} e^{j \omega t} \quad, \text { where } j=\sqrt{-1} \& \omega=2 \pi f
$$

Current $\quad I(\omega)=I_{o} \cos (\omega t-\varphi)$

$$
=I_{o} e^{j(\omega \theta-\varphi)}
$$

Impedance $\quad Z(\omega)=\frac{E(\omega)}{I(\omega)} \quad \leftarrow$ Ohm's Law

$$
\begin{aligned}
& =Z_{o}(\omega) e^{j \varphi(\omega)} \quad, \text { where } Z_{o}=E_{o} / I_{o} \\
& =Z_{o}(\cos \varphi+j \sin \varphi) \rightarrow \text { Modulus \& Phase }
\end{aligned}
$$

$$
=Z^{\prime}+j Z^{\prime \prime}
$$

(Bode Plot)
$\rightarrow$ Real \& Imaginary part (Nyquist Plot)

## Presentation of Impedance Spectrum

- Nyquist Plot
- Vectors of length |Z|
- Individual charge transfer processes are resolvable.
- Frequency is not shown.
- Small Z can be hidden by large Z.

- Bode Plot
- C may be determined graphically.
- Small Zs in presence of large Zs are usually easy to identify.




## Basic Circuit Elements



## Combinations of Elements

- Serial Combination
- Parallel Combination


$$
Z=Z_{1}+Z_{2}
$$



$$
\frac{1}{Z}=\frac{1}{Z_{1}}+\frac{1}{Z_{2}}
$$

## Combinations of Circuit Elements

R-C

$$
\longrightarrow W H \quad \rightarrow \quad Z=R+\frac{1}{j \omega C}
$$



## $\mathrm{R}_{5}-\mathrm{R} \mid \mathrm{C}$



1. $\omega \rightarrow 0, Z=R_{s}+R$
2. $\omega \rightarrow \infty, Z=R_{s}$
3. $Z=R_{S}+\frac{R}{1+\omega^{2} R^{2} C^{2}}, \quad Z^{\prime \prime}=-\frac{R \times \omega R C}{1+\omega^{2} R^{2} C^{2}} \quad \therefore\left\{Z-\left(R_{S}+\frac{R}{2}\right)\right\}^{2}+Z^{\prime 2}=\left(\frac{R}{2}\right)^{2}$
4. $Z=R_{s}+\frac{R}{2} \Rightarrow \frac{R \times \omega_{\max } R C}{1+\omega_{\max }^{2} R^{2} C^{2}}=\frac{R}{2}$
$\therefore \omega_{\max }=\frac{1}{R C} \Rightarrow-Z^{\prime \prime}=-Z^{\prime \prime}{ }_{\text {max }}, \quad \operatorname{phase} \varphi=\varphi_{\text {min }}$

## $R_{s}-\mathrm{R} \mid \mathrm{C}$



Phase $\varphi$


## Coating Capacitance

- Ideal Coating

$C_{\text {coat }}=\varepsilon \frac{A}{d}$
$\mathcal{W H}_{\mathrm{R}} \|_{\mathrm{C}_{\text {oot }}}$
- Imperfect Coating



## Uniqueness of Models

- There is not a unique equivalent circuit that describes a spectrum.
- Measuring $Z$ is simple and easy, but analyzing it is difficult.
- Physically relevant model is important.
- It can be tested by altering physical parameters.
- Be cautious in handling empirical models even if you get a good looking fit.
- Use the fewest elements


Same Impedance Spectrum


- Test it by T-test



## Disadvantages of EIS

- Ambiguities in interpretation
- All cells have intrinsically distributed properties
- Ideal circuit elements may be inadequate to describe real
electrical response
- Use of distributed elements (e.g. CPE)
- There is not a unique equivalent circuit describes measured impedance spectrum


## Advantages of EIS

- Relatively simple electrical measurement
- But analysis of complex material variables: mass transport, rates of chemical reactions, corrosion....
- Predictable aspects of the performance of chemical sensors and fuel cells
- Providing empirical quality control procedure



# Circuit Elements and Electrochemical Meanings 

## Physical Electrochemistry <br> \& Equivalent Circuit Elements

- Electrolyte Resistance
- 3 electrode: between WE and RE
- 2 electrode: all series $R$ in the cell are measured incld. $R$ of contacts, electrodes, solution, and battery separators
- Depends on ionic concentration, type of ions, temperature, and geometry


## Physical Electrochemistry <br> \& Equivalent Circuit Elements

- Charge Transfer Resistance
- Echem charge transfer reactions are generally modeled as resistances.
- When an EIS spectrum is measured on a corrosion cell at $\mathrm{E}_{\text {corrr }}$ the resistance at low-frequency is identical to the polarization resistance.

For a one step, multi-electron process, $O+n e \leftrightarrows R$ small overpotential is given by

$$
\eta=\frac{R T}{n F}\left[\frac{C_{O}(0, t)}{C_{o}^{*}}-\frac{C_{R}(0, t)}{C_{R}^{*}}+\frac{i}{i_{o}}\right]
$$

## Physical Electrochemistry \& Equivalent Circuit Elements



From A. J. Bard \& L. R. Faulkner, "Electrochemical Methods"

- Double Layer Capacitance
- A electrical double layer forms as ions from the solution "stick on" the electrode. There is an $\AA$-wide separation between charge in the electrode and ionic charges in the solution.
- Charges separated by an insulator form a capacity. On a bare metal, estimate 20 to $40 \mu \mathrm{~F}$ of C for every $\mathrm{cm}^{2}$ of electrode area.
- Depends on electrode potential, temperature, ionic concentrations, types of ions, oxide layers, electrode roughness, impurity adsorption, etc


## Physical Electrochemistry \& Equivalent Circuit Elements

- Constant Phase Element (CPE)
- The CPE is basically an imperfect capacitor.
- It's phase shift is less than $90^{\circ}$.

$$
Z_{C P E}=\frac{1}{A \times(j \omega)^{\alpha}}
$$

- Unlike C, a CPE has 2 parameters
- $\alpha$ is generally between 0.9 and 1.0
- A is similar to C
- Possible Explanations
- Surface roughness $\rightarrow$ Fractal Dimension, $D=1+1 / \alpha$

- Distribution of reaction rates on a surface
- Varying thickness or composition of a coating


## Physical Electrochemistry <br> \& Equivalent Circuit Elements

- Diffusion
- Diffusion processes can create an impedance, which is small at high frequency and increases as frequency decreases.
- Warburg Impedance
- Warburg looks like a special CPE with $A=1 / s$ and $\alpha=1 / 2$.
- However, remember that Warburg is derived from electrochemical kinetics. Parameters you obtain with Warburg have physical meanings. It is only partly true for CPE.
- You can get a good fit, but how to interpret the resulting parameters?

For a one-step, multi-electron process
$Z_{W}=\frac{\sigma}{\sqrt{\omega}}(1-j)=\frac{\sigma}{\sqrt{\omega}} e^{-\frac{\pi}{4} j}=\frac{\sigma}{(j \omega)^{1 / 2}} \quad \sigma=\frac{R T}{n^{2} F^{2} A \sqrt{2}}\left(\frac{1}{D_{O}^{1 / 2} C_{O}^{* *}}+\frac{1}{D_{R}^{1 / 2} C_{R}^{*}}\right)$

## Physical Electrochemistry

\& Equivalent Circuit Elements

- Diffusion
- Nernstian \& Finite Diffusion Impedance

$$
Z=\frac{\sigma}{\sqrt{\omega}}(1-j) \tanh (\delta \sqrt{j \omega / D}) \quad Z=\frac{\sigma}{\sqrt{\omega}}(1-j) \operatorname{coth}(\delta \sqrt{j \omega / D})
$$

- Homogeneous reaction (Gerischer) $\quad Z=\frac{1}{A \sqrt{B+j \omega}}$
- Spherical Diffusion

$$
Z=\frac{1}{A} \frac{1}{\sqrt{B}+\sqrt{j \omega}}
$$

## Physical Electrochemistry

\& Equivalent Circuit Elements

- Diffusion $\leftarrow$ Transmission Line Model

Warburg


Nernstian Impedance: Diffusion by Constant Concentration


$$
Z=\frac{\sigma}{\sqrt{\omega}}(1-j) \tanh (\delta \sqrt{j \omega / D})
$$

Finite Diffusion Impedance: Diffusion by Phase Boundary


$$
Z=\frac{\sigma}{\sqrt{\omega}}(1-j) \operatorname{coth}(\delta \sqrt{j \omega / D})
$$

## คM <br> $\mathrm{R}: 100 \Omega$ <br> C: 0.001F <br> Nernstian Impedance



## R <br>  <br> C: 0.001F <br> Nernstian Impedance



##  <br> Finite Diffusion Impedance



##  <br> Finite Diffusion Impedance



## Validation of Impedance Data Kramers-Kronig Relation

## Validation of Impedance Data

- Ideal impedance data must fulfill:
- Causality: The output must be exclusively a result of the input
- Linearity: The response must be a linear fn. of the perturbation
- Stability: The system must not be changing during measurement
$\rightarrow$ a serious problem for corroding systems
- Finite-Valued: Impedance must be finite value at any frequency
- Kramers-Kronig Relation:
- Validation Test
- Low Frequency Extrapolation

$$
\text { a. } \mathrm{Z}^{\prime \prime} \rightarrow \mathrm{Z}^{\prime}
$$

$$
Z^{\prime}(\omega)=Z^{\prime}(\infty)+\frac{2}{\pi} \int_{0}^{\infty} \frac{x Z^{\prime \prime}(x)-\omega Z^{\prime \prime}(\omega)}{x^{2}-\omega^{2}} d x
$$

- The integration range includes the frequencies zero and infinity
- Note pure capacitor cannot be calculated
b. $Z^{\prime} \rightarrow Z^{\prime \prime}$

$$
Z^{\prime \prime}(\omega)=-\frac{2 \omega^{\infty}}{\pi} \int_{0}^{\infty} \frac{Z^{\prime}(x)-Z^{\prime}(\omega)}{x^{2}-\omega^{2}} d x
$$

## Electrochemistry: A Linear System?



- Circuit theory is simplified when the system is "linear".
- Z in a linear system is independent of excitation amplitude. The response of a linear system is always at the excitation frequency (no harmonics are generated).
- Look at a small enough region of a current versus voltage curve and it becomes linear.
- If the excitation is too big, harmonics are generated and EIS modeling does not work.


## E'chem: A Stationary System?

- Measuring EIS spectrum takes time (often many hours).
- The sample can change during the time the spectrum is recorded.
- If this happens, modeling results may be wildly inaccurate.
- To shorten the measuring time of impedance spectrum, use FFT EIS method.

Non-Stationary Conditions result in non-stationary spectra!

## Validation of Impedance Data Z-HIT

## Limitation of K-K Relation

- The integration range includes the frequencies zero and infinity
- |Z| and Phase are measured independently with different accuracy and sensitivity, but in theory, they are correlated with each other.



## Z-HIT Approximation

$$
\ln \left|Z\left(\omega_{0}\right)\right| \approx \text { const. }+\frac{2}{\pi} \int_{\omega_{s}}^{\omega_{0}} \varphi(\omega) d \ln \omega+\gamma \cdot \frac{d \varphi\left(\omega_{o}\right)}{d \ln \omega}
$$

Local relationship between impedance and phase
=> Not affected by the limited bandwidth problem
=> Reliable detection of artifacts and instationarities (drift)
=> Reconstruction (!!) of causal spectra
=> Reliable interpretation of spectra

## Other Methods to Measure EIS

## Multi-Sine Wave Method



## Others

## Inductive Loop at High Frequency

- The effects of inductances are often seen at the high frequencies
- The value of inductor is very small, however, this can be important if the electrode impedance is low.
- Possible Causes

- Actual physical inductance of loop or coil of wire between electrode and potentiostat
- Self inductance of the electrode itself: even a straight piece of rod has some self inductance ~ several nH
- Some cylinder-type batteries also shows this effect ~ uH
- Instrumental artifacts, notably capacitance associated with the current measuring resistor, however. potentiostat manufacturers may have already made corrections for this effect



## Galvanostatic EIS is Better for Low Z

- Potentiostatic Mode
- Vac is 1 mV Minimum !
$-1 \mathrm{mV}_{\mathrm{rms}}=1.414 \mathrm{~A}_{\mathrm{rms}} \times Z$
$-Z_{\text {min }}=707 \cup \Omega$
- These are Absolute Minimum Z Values!
- Limitation is APPLIED E
- Measured E is still Accurate!
- Galvanostatic Mode
- Can Measure Smaller E Values !~Microvolts
- CMR of electrometer may limit the absolute minimum Z Values! -> 5 U $\Omega$
- Refer to "Shorted Lead Test"


## How to Extract Model Parameters

- Building equivalent circuit model
- Physically relevant model
- Each component is postulated to come from a physical process in the EChem cell based on knowledge of the cell's physical characteristics.
- Empirical model
- Complex Nonlinear Least Square (CNLS) Fitting Algorithm
- is used to find the model parameters that cause the best agreement between a model's impedance spectrum and a measured spectrum.
- starts with initial estimates of model parameters.
- Iterations continue until the goodness of fit exceeds an acceptance criterion, or until the number of iterations reaches a limit.
- Please check the change of $\chi^{2}$ after each iteration.
- Sometimes, CNLS algorithm cannot converge on a useful fit because of
- An incorrect model
- Poor estimates for the initial values
- Noise and etc.
- Don't care if the fit looks poor over a small section of the spectrum.

